SECTION G2

PROTECTION AND CONTROL REQUIREMENTS FOR GENERATION ENTITIES

PG&E GENERATION INTERCONNECTION HANDBOOK

PURPOSE

This section specifies the requirements for protective relays and control devices for Generation Entities interconnecting to the PG&E Power System.

APPLICABILITY

The applicable protective standards of this section apply to all Generators interconnecting to any portion of the PG&E’s Transmission Power System, except those that qualify for treatment under the CPUC Rule 21. These standards, which govern the design, construction, inspection and testing of protective devices, have been developed by PG&E to be consistent with Applicable Regional Reliability Criteria and to include appropriate CAISO consultation. The CAISO, in consultation with PG&E, may designate certain new or existing protective devices as CAISO Grid Critical Protective Systems. Such systems have special CAISO requirements, e.g., for installation and maintenance, as described in the CAISO Tariff Section 5 and the TCA Section 8.

In the future, the CAISO may develop its own standards or requirements applicable to certain interconnections, and also will review and comment on interconnection requests to the CAISO Controlled Grid. Refer to the Introduction of this handbook.

In addition, for Generation Entities connecting directly to a Third Party: A third party must coordinate with the CAISO, PG&E (as the Transmission Owner), and the Generation Entity, as needed, to ensure that any CAISO Controlled Grid Critical Protective Systems, including relay systems, are installed and maintained in order to function on a coordinated and complementary basis with the protective systems of the Generation Entity and the PG&E Power System, in accordance with the CAISO Tariff Section 4 and the CAISO-UDC Agreement, both available on the CAISO website.

1 See Glossary for more information. NERC reliability standards for transmission voltage levels of 100kV and above require the use of two separate voltage and current sources to be connected to the primary and alternate line protective relays respectively. Conformance to WECC and NERC standards are required for interconnections above 100kV voltage levels.
G2.1 PROTECTIVE RELAY REQUIREMENTS

An important objective in the interconnection of facilities to the PG&E Power System is minimizing the potential hazard to life and property. A primary safety requirement is the ability to disconnect immediately when a fault is detected.

The protection equipment for a generation facility must protect against faults within that facility and faults on the PG&E Power System. A generation facility must also trip off-line (disconnect from the PG&E Power System automatically) when PG&E’s power is disconnected from the line into which the unit is generating.

In view of these objectives, PG&E requires line-protective equipment to either: 1) automatically clear a fault and restore power, or 2) rapidly isolate only the faulted section so that the minimum number of customers are affected by any outage.

Due to the high energy capacity of the PG&E transmission system, high-speed fault clearing may be required, to minimize equipment damage and potential impact to system stability. The requirement of high-speed fault clearing will be determined by PG&E on a case-by-case basis. To achieve these results, relays and protective devices are needed. The requirements are outlined in the following pages and in Appendix R. Some protection requirements can be standardized; however, most line relaying depends on generator size and type, number of generators, line characteristics (i.e., voltage, impedance, and ampacity), and the existing protection equipment connected to the PG&E Power System.

Identical generator projects connected at different locations in the PG&E Power System can have widely varying protection requirements and costs. These differences are caused by different line configurations, fault duties and existing relay schemes. See Appendix S for more information.

PG&E's protection requirements are designed and intended to protect the PG&E Power System only. As a general rule, neither party should depend on the other for the protection of its own equipment.

The Generation Entity shall install at the Point of Interconnection, at a minimum, a disconnecting device or switch with generation interrupting capability. Additional protective relays are typically needed to protect the Generation Entity’s facility adequately. It is the Generation Entity’s responsibility to protect its own system and equipment from faults or interruptions originating on both PG&E’s side and the Generation Entity’s side of the Interconnection. The Generation Entity’s System Protection Facilities shall be designed, operated, and maintained to isolate any fault or abnormality that would adversely affect the PG&E Power System or the systems of other entities connected to the PG&E Power System. The Generation Facility shall, at its expense, install, operate, and maintain system protection facilities in accordance with applicable CAISO, WECC and NERC requirements and in accordance with design and application requirements of this Handbook.

The protective relays used in isolating the Generation Facility from the PG&E Power System at the Point of Interconnection must be PG&E-approved devices and must be set to coordinate with the protective relays at the PG&E line breaker terminals for the line on which the Generation Facility is connected. Additional requirements, as to the exact type and style of the protective devices, may be imposed on the Generation Entity based on the proposed station configuration or the type of interrupting device closest to the point of common coupling to PG&E’s facility. Note: There may be additional protective equipment requirements, at the Generation Entity’s cost, which PG&E will coordinate with the Generation Entity or its representatives.

PG&E recommends that the entity acquire the services of a qualified electrical engineer to review the electrical design of the proposed generation facility and ensure that it will be adequately protected.

The required types of protective devices are listed on Tables G2-1a and G2-1b. Typical protection and metering installations are shown on Figures G1-1 and G1-2 in Section G1.
Generally, fault-interrupting equipment should be located as close to the interconnection point as possible - typically within one span of overhead line or 200 feet of unspliced underground cable.

The Generation Entity should provide PG&E with electrical drawings for review prior to equipment procurement. The drawings provided should consist of Single Line Meter and Relay Diagrams, schematic drawings detailing connectivity (3-Line AC) and tripping schemes (DC) for all PG&E required relays. The Single Line Meter and Relay Diagrams listing the major protective equipment should be provided prior to ordering relays. The 3-Line AC and the DC schematics should be provided before fabricating relay panels. The following documents must be submitted for review before any agreements are executed: Single Line Diagram, Single Line Meter and Relay Diagrams.

It is critical to the project schedule that the required leased circuits are ordered many months in advance of the operational date. In Appendix F the timeframes are provided for different types of circuits and services. These are approximate lead times since each facility will have to be evaluated by the telephone company to determine the availability of adequate cable pair facilities for the required service. If the requisite cable plant is not available, the project timeline may be extended 6 to 12 months. The required leased circuits must be in place before a company may generate electricity into the PG&E power grid.

The Generation Entity must provide PG&E with test reports (Form G2-2) for the particular types of protective devices applied as outlined in Tables G2-1a and G2-1b before PG&E will allow the facility to parallel. Where tele-protection is utilized, the communication circuits must be tested and the scheme operation functionally verified prior to release for commercial operation. Refer to Pre-parallel Inspection for Generation Customers, Section G5, for information regarding pre-parallel inspections and Appendix F for communication-assisted line protection. Every four years thereafter, the Generation Entity must submit written test reports for qualified testing to PG&E, that demonstrate the relays are operable and within calibration. PG&E will not test the entity's equipment, but may witness the testing performed by a qualified testing firm retained by the entity. On-site power (typically 120 volts) is required for the test equipment. Circuit breakers must be tested at least every eight years after the pre-parallel inspection. It is also in the Generation Entity’s best interest to make sure all of its protective equipment is operating properly, since significant equipment damage and liability can result from failures of the entity’s protective equipment. Refer to the Operation Procedures, Section G4, of this handbook for the requirements on reporting relay problems. At the same four-year interval as the relay testing, the Generation Entity should obtain confirmation from the appropriate telephone company that the leases for the protection circuits are configured properly (e.g. Mutual Drainage Reactors installed at Central Office or Remote Terminal).

G2.2 RELIABILITY AND REDUNDANCY

The Generation Entity shall design the protection system with sufficient redundancy that the failure of any one component will still permit the Generation Entity’s facility to be isolated from the PG&E Power System under a fault condition. Multi-function three-phase protective relays must have redundant relay(s) for back-up. The required breakers must be trip tested by the Generation Entity at least once a year. It is PG&E’s practice to use two relays from different manufacturers in order to provide adequate level of redundancy and security and to avoid single mode of failure for both levels of protection. Any customer interface protective devices that have potential impact on PG&E system will have to comply with this practice regardless of transmission line ownership. Protection of customer-owned equipment by two relays from the same vendor is acceptable as long as these relays

2 Refer to Appendix F for recommendations and requirements associated with pilot protection.
3 Submittal of these drawings is required before a Generation Entity is allowed to parallel with the PG&E Power System.
4 Communication-assisted protection tests include end-to-end satellite testing of the protection and communication between the interconnected terminals as a system. See Appendix F for more information.
utilize different operating principles. An example of relays requiring redundancy would be the intertie breaker and the main customer transformer protection. PG&E strongly recommends against using fuses for protection of DC control and protection circuits, since they could fail open without indication resulting in disabling of protection and controls including breaker tripping. If fuses are used in trip circuits, trip coil monitoring and alarming must be used.
G2.3 RELAY GRADES

Only utility grade relays can be used for interconnection protection.

These relays, used by electric utilities, have much higher reliability and accuracy than industrial grade relays (see Tables G2-4 and G2-5). In addition, they typically have draw-out cases and indicating targets or better recording to facilitate testing and troubleshooting.

All utility grade relays must include manually resettable relay targets.

All relays must have 5A nominal AC input current.

All utility grade relay power supplies must be powered by station battery DC voltage, and the battery system should include a DC undervoltage detection device and alarm. See Section G2-20 and Appendix T (Battery Requirements for Interconnection to PG&E System).

All proposed relay specifications must be submitted to PG&E for approval prior to ordering. Line protection relays must come from PG&E’s approved list (See G2-4 and G2-5). Generation protection relays can come from PG&E’s approved list G2-4 and G2-5 or the Generation Entity can have testing performed to qualify relays in accordance with the Appendix R - “Generation Protective Relay Requirements”. Any required qualified tests shall be performed at the Generation Entity’s expense and prior to PG&E approval of the relay for interconnection use. PG&E approval does not indicate the quality or reliability of a product or service, and endorsements or warranties shall not be implied. If the entity wants to use a relay not on the PG&E approved list (Tables, G2-4 and G2-5) the entity should allow additional time for testing and approval.

G2.4 LINE PROTECTION

Line-protection relays must coordinate with the protective relays at the PG&E breakers for the line on which the generating facility is connected. The typical protective zone is a two-terminal line section with a breaker on each end. In the simplest case of a load on a radial line, current can flow in one direction only, so protective relays need to be coordinated in one direction and do not need directional elements. However, on the typical transmission system, where current may flow in either direction depending on system conditions, relays must be directional. Also, the complexity and the required number of protective devices increase dramatically with increases in the number of terminals in each protective zone. With two terminals in a protective zone, there are two paths of current flow. With three terminals there are six paths of current flow, and so on.

In coordinating a multi-terminal scheme, PG&E may require installation of a transmission line protective relay at the Generation Entity’s sub-site. This is commonly the case whenever three-terminal permissive overreach transfer trip (POTT) schemes are employed to protect the line. Because this line relay participates in a scheme to protect the PG&E transmission system, PG&E must ensure the maintenance, testing and reliability of this particular type of relay.

The relays must be connected to the breaker CTs in such a way that zones of protection overlap. The line protection schemes must be able to distinguish between generation, inrush and fault currents. Multiple terminal lines become even more complex to protect. Existing relay schemes may have to be reset, replaced, or augmented with additional relays at the Generation Entity’s expense, to coordinate with the Generation Entity’s new facility.

The PG&E required relays must be located so that a fault on any phase of the PG&E interconnected line(s) shall be detected. If transfer trip protection is required by PG&E, the Generation Entity shall provide all required communication circuits at its expense. A communication circuit may be a leased line from the telephone company, a dedicated cable,
microwave, or a fiber optic circuit and shall be designed with sufficient levels of monitoring of
critical communication channels and associated equipment. PG&E will determine the appropriate
communication medium to be used on a case-by-case basis. The leased phone line or dedicated
communication network must have high-voltage protection equipment on the entrance cable so
the transfer trip equipment will operate properly during fault conditions. (Refer to Appendix F
for a detailed description of protection requirements and associated transfer trip equipment and
communications circuits monitoring.)

The PG&E transmission system and the distribution network system are designed for high
reliability by having multiple sources and paths to supply customers. Due to the multiple sources
and paths, more complex protection schemes are required to properly detect and isolate the faults.
The addition of any new generation facility to the PG&E Power System must not degrade
the existing protection and control schemes or cause existing PG&E customers to suffer
lower levels of safety and/or reliability (see Electric Rule 2).

Many portions of the PG&E Power System have provisions for an alternate feed. In some
locations, the generation cannot be allowed on line while being fed from an alternate source due
to protection problems. Whenever possible, the Generation Entity will be given the option of
paying for any required upgrades so that they can stay on line while transferred to the alternate
source or not paying for upgrades and accepting shutdowns when transferred to the alternate
source.

Table G2-1a lists the minimum protection that PG&E typically uses on its own installations.
Higher voltage interconnections require additional protection due to the greater potential for
adverse impact to system stability, and the greater number of customers who would be affected.
Special cases such as distribution-level network interconnections, if acceptable, may have
additional requirements. The acceptability and additional requirements of these interconnection
proposals shall be determined by PG&E on a case-by-case basis.
### Line Protection Devices

<table>
<thead>
<tr>
<th>Line Protection Device</th>
<th>Device Number</th>
<th>34.5kV or less</th>
<th>44kV, 60kV or 70kV</th>
<th>115kV</th>
<th>230kV</th>
</tr>
</thead>
<tbody>
<tr>
<td>Phase Overcurrent (Radial systems)</td>
<td>50/51</td>
<td>X</td>
<td>X</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Ground Overcurrent (Radial systems)</td>
<td>50/51N</td>
<td>X</td>
<td>X</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Phase Directional Overcurrent</td>
<td>67</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Ground Directional Overcurrent or Transformer Neutral</td>
<td>67N 50/51N</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Distance Relay Zone 1 (phase and ground elements where applicable)</td>
<td>21Z1 / 21 Z1N</td>
<td>X</td>
<td>X</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Distance Relay Zone 2 (phase and ground elements where applicable)</td>
<td>21Z2 / 21 Z2N</td>
<td>X</td>
<td>X</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Distance Relay Carrier</td>
<td>21Z2C</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Ground Directional Overcurrent Carrier</td>
<td>67NC</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Distance Relay Carrier Block</td>
<td>21Z3C</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Pilot Wire, Current differential, and Phase Comparison</td>
<td>87L/78</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Permissive Overreaching Transfer Trip (POTT) or Hybrid</td>
<td>21/67T</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Direct Transfer Trip</td>
<td>TT</td>
<td></td>
<td></td>
<td>X</td>
<td>X</td>
</tr>
</tbody>
</table>

**Notes:**

1. May be required on transmission or distribution interconnections depending on local circuit configurations, as determined by PG&E.

2. Transfer trip may be required on transmission-level or distribution-level interconnections depending on PG&E circuit configuration and loading, as determined by PG&E. Typically, transfer trip shall be required if PG&E determines that a generation facility cannot detect and trip on PG&E end-of-line faults within an acceptable time frame, or if the generation facility may be capable of keeping a PG&E line energized with the PG&E source disconnected (Appendix F).

3. Refer to Table G2-1 for device number definitions and functions.

4. Line protection application is a function of the power system parameters and equivalent sources to which equipment are interconnected given the rating of the equipment being installed for interconnection purposes.

5. All relays must have 5A nominal AC input current.

### G2.5 GENERATOR PROTECTION AND CONTROL

Single-phase generators must be connected in multiple units so that an equal amount of generation capacity is applied to each phase of a three-phase circuit.

All synchronous, induction and single-phase generators shall comply with the latest ANSI Standards C50.10 and C50.13, dealing with waveform and telephone interference.

Synchronous generators of any size will require: a) synchronizing relays, synch check, or auto synchronizer (Device No. 25) to supervise generator breaker closing, and b) reclose blocking at the PG&E side of the line to which the generator is connected (applies to substation...
breaker/recloser and line reclosers). Standard device numbers for commonly used protective elements are defined in Table G2-1.

The generator protection equipment listed in Table G2-1b, in addition to those listed in Table G2-1a, is required to permit safe and reliable parallel operation of the Generation Entity’s equipment with the PG&E Power System. Additional generator protection requirements shall be determined by PG&E on a case-by-case basis.

### Table G2-1b
**Generator Protection Devices**

<table>
<thead>
<tr>
<th>Generator Protection Device</th>
<th>Device Number</th>
<th>40 kW or Less</th>
<th>41 kW to 400 kW</th>
<th>401 kW and Larger</th>
</tr>
</thead>
<tbody>
<tr>
<td>Phase Overcurrent</td>
<td>50/51</td>
<td>X^2</td>
<td>X^2</td>
<td></td>
</tr>
<tr>
<td>Overvoltage</td>
<td>59</td>
<td>X</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Undervoltage</td>
<td>27</td>
<td>X^1</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Overfrequency</td>
<td>81O</td>
<td>X</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Underfrequency</td>
<td>81U</td>
<td>X</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Ground Fault Sensing Scheme (Utility Grade)</td>
<td>51N</td>
<td>X^4</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td>Overcurrent With Voltage Restraint/Voltage Control or Impedance Relay</td>
<td>51V</td>
<td>X^5</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td>Reverse Power Relay (No Sale)</td>
<td>32</td>
<td>X^6</td>
<td>X^6</td>
<td>X^6</td>
</tr>
</tbody>
</table>

**Notes:**

1. Refer to Table G2-1 for device number definitions and functions.
2. Overcurrent protection must be able to detect a line-end fault condition. A phase instantaneous overcurrent relay that can see a line fault under sub-transient conditions is required. This is not required if a 51V relay is used.
3. For generators 40 kW or less, the undervoltage requirement can be met by the contactor undervoltage release.
4. For induction generators and certified non-islanding inverters aggregating less than 100 kW, ground fault detection is not required. Ground fault detection is required for non-certified induction generators of 100kW or larger capacity. For synchronous generators aggregating over 40 kW, and induction generators aggregating over 100kV, ground fault detection is required.
5. A group of generators, each less than 400 kW but whose aggregate capacity is 400 kW or greater, must have an impedance relay or an overcurrent relay with voltage restraint located on each generator greater than 100 kW.
6. For “No Sale” generator installations, under the proper system conditions, a set of three single-phase, very sensitive reverse power relays, along with the dedicated transformer may be used in lieu of ground fault protection. The relays shall be set to pick-up on transformer magnetizing current, and trip the main breaker within 0.5 second.
7. All relays must have 5A nominal AC input current.

The following paragraphs describe the required protective and control devices for generators:

**G2.5.1 Phase Overcurrent**

See Table G2-1 (Device 50/51) for definition and function.
G2.5.2 Over/Undervoltage Relay

This protection is used to trip the circuit breaker when the voltage is above or below PG&E's normal operating level (see Table G2-6). It is used for generator protection and backup protection in the event that the generator is carrying load that has become isolated from the PG&E Power System.

G2.5.3 Over/Underfrequency Relay

This protection is used to trip the circuit breaker when the frequency is above or below PG&E's normal operating level (see Table G2-6). It is used for generator/turbine protection and backup protection.

Generator underfrequency relay settings are coordinated with other utilities in the Western Electricity Coordinating Council (WECC) to maintain generation on line during system disturbances. Settings should not be set for a higher frequency or shorter time delay than specified in Table G2-6 without prior written approval by PG&E and the CAISO.

G2.5.4 Ground Fault Sensing Scheme

G2.5.4.1 General:

The ground fault sensing scheme detects PG&E Power System ground faults and trips the generator breaker or the generating facility’s main circuit breaker, thus preventing the Generation Entity’s generator from continuously contributing to a ground fault. This scheme must be able to detect faults between the PG&E system side of the dedicated transformer and the end of PG&E's line. The following transformer connections, along with appropriate relaying equipment, are commonly used to detect system ground faults:

- System side - grounded wye; generator side - delta
- System side - grounded wye; generator side - wye; tertiary - delta

G2.5.4.2 Ground Grid Requirements

Transformers connected to the transmission system at 60 kV and higher must have a grounded wye connection on the system side, and a ground current sensing scheme must be used to detect ground faults on the PG&E Power System.

For any substation/generation facility built by other entities but subsequently owned and/or operated by PG&E, the ground grid must meet the minimum design and safety requirements used in PG&E substations. The ground grid design must by analyzed in accordance with the Grounding Design Criteria (Appendix E), and documented in accordance with PG&E Analysis Specification (Appendix E).

Additionally, when customer facilities (operated by customer personnel) need to be connected to the ground grid of an existing or new PG&E substation (i.e. when they are located inside or immediately adjacent to PG&E substations or switching stations OR when system protection requires solid ground interconnection for relay operation), the ground grid must meet the minimum design and safety requirements used in PG&E substations. (Appendix E)

When customer facilities are not in any way connected to the PG&E ground grid or neutral system, the customer will be solely responsible for establishing design and safety limits for their grounding system.
G2.5.5 Overcurrent Relay with Voltage Restraint/Voltage Control or Impedance Relay

These relays are used to detect multi-phase faults and initiate a generator circuit breaker trip. The relays must be located on the individual generator feeder. A group of generators aggregating over 400 kW must have an impedance relay or an overcurrent relay with voltage restraint located on each generator greater than 100 kW. Generators equal to or greater than 400 kW must have an impedance relay or an overcurrent relay with voltage restraint. As determined by PG&E protection studies, an overcurrent relay with voltage control may also be acceptable if it can be set to adequately detect end-of-line faults. If the generator step-up transformer is connected wye-delta or delta-wye, a delta-wye or wye-delta auxiliary potential transformer is required on the potential circuits to the voltage restraint or voltage controlled overcurrent relay for phase shift correction based on the relay design and operating principal. The Generation Entity should contact the PG&E representative for assistance in the proper connection of the auxiliary transformers.

G2.5.6 Reverse Power Relay

See Table G2-1b (Device #32) for definition and function.

G2.6 DEDICATED TRANSFORMER

A dedicated transformer is required to step-up the generator voltage to the interconnection level and isolate the Generation Entity from other customers.

The impedance of a dedicated transformer limits fault currents on the generator bus from the PG&E Power System and also limits fault currents on the PG&E Power System from the generator. Hence, it reduces the potential damage to both parties due to faults. It also must have a delta winding to reduce the generator harmonics entering the PG&E Power System. The delta winding will also reduce the PG&E Power System harmonics entering the generation facility.

A high-side fault-interrupting device is required for transformer protection. A three-phase circuit breaker is recommended, but fuses are acceptable for generation facilities of less than 1,000 kW, providing that coordination can be obtained with the existing PG&E protection equipment. If fuses are used, it is recommended that the Generation Entity install single-phase protection for its equipment.

Lightning arrestors, if the Generation Entity chooses to install them, must be installed between the transformer and the fault-interrupting devices and be encompassed by the generator’s relay protection zone.

G2.7 MANUAL DISCONNECT SWITCH

G2.7.1 General

A manual disconnect switch is required for a generation facility. For connections to the PG&E transmission grid, a tap line switch may also be required if, in PG&E’s judgment, sufficient tap line exposure exists to warrant it. Refer to section Appendix O for more details on tap line switches. For transmission line taps, two additional line selector switches, one on each side of the tap, are also recommended to provide the facility better service and operating flexibility. Refer to Appendix O for more details on line selector switches. Note: the installation of line selector switches may impact the protection requirements for the interconnection, specifically the need for direct transfer trip.

A PG&E-operated disconnect device must be provided as a means of electrically isolating the PG&E Power System from the generator. This device shall be used to establish visually open working clearance for maintenance and repair work in accordance with PG&E safety rules and practices. A disconnect device must be located at all points
of interconnection with PG&E. The disconnect switch should be a gang-operated, three-pole lockable switch.

If the switch is to be located on the PG&E side of the interconnection point, PG&E will install the switch at the Generation Entity’s expense. If the device is to be located on the entity’s side, it must be furnished and installed by the Generation Entity. All switch devices must be approved by PG&E. PG&E personnel shall inspect and approve the installation before parallel operation is permitted. If the disconnect device is in the Generation Entity’s substation, it should be located on the substation dead-end structure and must have a PG&E-approved operating platform.

The disconnect device must not be used to make or break parallels between the PG&E Power System and the generator(s). The device enclosure and operating handle (when present) shall be kept locked at all times with PG&E padlocks.

The disconnect device shall be physically located for ease of access and visibility to PG&E personnel. When installed on the Generation Entity’s side of the interconnection, the device shall normally be installed close to the metering. The PG&E-operated disconnect shall be identified with a PG&E designated switch number plate.

Metering is normally on the high-side of the Generation Entity’s step-up transformers. Between the metering units and the circuit breaker, a second disconnect device is required; it shall not have a PG&E lock and may be operated by the Generation Entity.

G2.7.2 Specifications

- Disconnect switches must be rated for the voltage and current requirements of the particular installation
- Disconnect switches must be gang-operated
- Disconnect switches must be weatherproof or designed to withstand exposure to weather
- Disconnect switches must be lockable in both the open/closed positions with a standard PG&E lock.

G2.8 FAULT-INTERRUPTING DEVICES

The fault-interrupting device selected by the Generation Entity must be reviewed and approved by PG&E for each particular application.

There are two basic types of fault-interrupting devices:

- Circuit Breakers
- Circuit Switchers

PG&E will determine the type of fault-interrupting device required for a generation facility based on the size and type of generation, the available fault duty, the local circuit configuration, and the existing PG&E protection equipment.

G2.8.1 Circuit Breakers

A three-phase circuit breaker at the point of interconnection automatically separates the generation facility from the PG&E Power System upon detection of a circuit fault. Additional breakers and protective relays may be installed in the generation facility for ease in operating and protecting the facility, but they are not required for the purpose of interconnection. The interconnection breaker must have sufficient capacity to interrupt maximum available fault current at its location and be equipped with accessories to:
• Trip the breaker with an external trip signal supplied through a battery (shunt trip)
• Telemeter the breaker status when it is required
• Lockout if operated by protective relays required for interconnection

Generally, a three-phase circuit breaker is the required fault-interruption device at the point of interconnection, due to its simultaneous three-phase operation and ability to coordinate with PG&E line-side devices.

### G2.8.2 Circuit Switchers

A circuit switcher is a three-phase fault-interrupter with limited fault interrupting capability. These devices have typically been used at voltages of 115 kV and below and may substitute for circuit breakers when the fault duty is within the interrupting rating of the circuit switcher. With PG&E approval, some circuit switchers with blades can double as the visual open disconnect switch between the metering transformers and the main transformer. Since circuit switchers do not have integral current transformers, they must be installed within 30 feet of the associated current transformers to minimize the length of the unprotected line/bus section.

### G2.9 SYNCHRONOUS GENERATORS

The generating unit must meet all applicable American National Standards Institute (ANSI) and Institute of Electrical and Electronic Engineers (IEEE) standards. The prime mover and the generator should also be able to operate within the full range of voltage and frequency excursions that may exist on the PG&E Power System without damage to themselves. The generating unit must be able to operate through the specified frequency ranges for the time durations listed in Table G2-6, to enhance system stability during a system disturbance.

#### G2.9.1 Synchronizing Relays

The application of synchronizing devices attempts to assure that a synchronous generator will parallel with the utility electric system without causing a disturbance to other customers and facilities (present and in the future) connected to the same system. It also attempts to assure that the generator itself will not be damaged due to an improper parallel action. Refer to Appendix Q for additional information and requirements.

Synchronous generators and other generators with stand-alone capability must use one of the following methods to synchronize with the PG&E Power System:

**G2.9.1.1 Automatic Synchronizers Approved by PG&E See Table G2-4 for PG&E-approved devices.**

Automatic synchronization with automatic synchronizer (Device 15/25) to synchronize with the PG&E Power System. The automatic synchronizer must be approved by PG&E and have all of the following characteristics:

- Slip frequency matching window of 0.1 Hz or less
- Voltage matching window of ± 10 percent or less
- Phase angle acceptance window of ± 10 degrees or less
- Breaker closure time compensation. For an automatic synchronizer that does not have this feature, a tighter phase angle window (± 5 degrees) with a one second time acceptance window shall be used to achieve synchronization within ± 10 degrees phase angle
Note: The automatic synchronizer has the ability to adjust generator voltage and frequency automatically to match system voltage and frequency, in addition to having the above characteristics.

G2.9.1.2 Automatic Synchronizers (not on PG&E’s approved list) Supervised by a PG&E-Approved Synchronizing Relay

Automatic synchronization with a device not approved by PG&E supervised by an approved synchronizing relay (Device 25). The synchronizing relay must have all of the following characteristics:

- Slip frequency matching window of 0.1 Hz or less
- Voltage matching window of ± 10 percent or less
- Phase angle acceptance window of ± 10 degrees or less
- Breaker closure time compensation

Note: The synchronizing relay closes a supervisory contact after the above conditions are met, allowing the non-approved automatic synchronizer to close the breaker.

G2.9.1.3 Manual Synchronization Supervised by a Synchronizing Relay

Manual synchronization with supervision from a synchronizing relay (Device 25) to synchronize with the PG&E Power System. The synchronizing relay must have all of the following characteristics:

- Slip frequency matching window of 0.1 Hz or less
- Voltage matching window of ± 10 percent or less
- Phase angle acceptance window of ± 10 degrees or less
- Breaker closure time compensation

Note: The synchronizing relay closes a supervisory contact, after the above conditions are met, allowing the breaker to close.

G2.9.1.4 Manual Synchronization With Synch-Check Relay

Manual synchronization with synchroscope and synch-check (Device 25) relay supervision. (Only allowed for generators with less than 1000 kW aggregate nameplate rating). The synch-check relay must have the following characteristics:

- Voltage matching window of ± 10 percent or less.
- Phase angle acceptance window of ± 10 degrees or less.

Generators with greater than 1,000 kW aggregate nameplate rating must have a synchronizing relay or automatic synchronizer.

G2.9.2 Frequency/Speed Control

Unless otherwise specified by PG&E, a governor shall be required on the prime mover to enhance system stability. Governor characteristics shall be set to provide a 5 percent droop characteristic. Governors on the prime mover must be operated unrestrained to help regulate PG&E’s system frequency.

G2.9.3 Excitation System Requirements

An excitation system is required to regulate generator output voltage.
Excitation systems shall have a minimum ceiling voltage of 150 percent of rated full load field voltage and be classified as a high initial response excitation system as defined in IEEE 421.1. Static Systems shall meet these criteria with 70 percent of generator terminal voltage. The offline generator terminal voltage response shall have an overshoot limited to 20 percent and a bandwidth of at least 0.1 to 4 hertz. However, in no case shall the bandwidth upper limit be less than local mode frequency. All systems shall be suitable to utilize a Power System Stabilizer as described in G2.9.4.

Ceiling current shall have a transient time capability equal to or greater than the short time overload capability of the generator. See ANSI C50.12, 13, or 14.

A means shall be provided to quickly remove excitation from the generator field to minimize contributions to faults. The preferred method is to reverse voltage the generator field to drive the current to zero.

Excitation systems shall respond to system disturbances equally in both the buck and boost directions. All bridges that govern excitation response shall be full wave type. Bridges feeding a pilot exciter shall have negative forcing capability.

Under certain conditions PG&E may grant an exemption for Generating Facilities that have excitation systems not meeting these requirements. Requests for exemption should be sent to PG&E’s Electric T&D Engineering at the following address:

Director, Electric T&D Engineering
Pacific Gas and Electric Co.
Mail Code H12A
P.O. Box 770000
San Francisco, CA 94177

G2.9.4 Voltage Regulator
Voltage control is required for all synchronous generators interconnected at transmission level voltages.

The regulator must be acting continuously and be able to maintain the generator voltage under steady-state conditions without hunting and within \( \pm 0.5\% \) percent of any voltage level between 95 percent and 105 percent of the rated generator voltage per CAISO requirements. The point of voltage sensing should be at the same point as the PG&E revenue metering.

Voltage regulators shall have a minimum of the following signal modifiers:

- Reactive current compensator capable of line drop or droop characteristic
- Minimum and maximum excitation limiter
- Volts per Hertz limiter
- Two levels of over-excitation protection. The first level should provide a forcing alarm and trip the voltage regulator after a time delay. The second level shall have an inverse time characteristic such that the time-current relationship may be coordinated with the generator short time thermal requirements (ANSI C50.13 or C50.14).
- A two input Power System Stabilizer (PSS) utilizing Integral of Accelerating Power to produce a stabilizing signal to modify regulator output. The PSS shall be an integral part of the voltage regulator and be incorporated into the excitation systems for all generating units greater than 30 MVA and connected to the transmission system at 60 kV and greater. PG&E can help determine, at the Generation Entity’s
expense, the suitability of an excitation system for PSS. The PSS shall provide a positive contribution to damping for a frequency range from 0.1 hertz through local mode frequency.

Voltage schedules will be determined by the Designated Electric Control Center, in coordination with the Transmission Operations Center and the CAISO.

At various times, the generating facility may also be requested by the Designated Electric Control Center, in coordination with the ISO, to produce more or less reactive power from that indicated on the regular schedule in order to meet the system needs.

**G2.9.5 Power Factor Controller**

The controller must be able to maintain a power factor setting within ±1 percent of the setting at full load at any set point within the capability of the generator. However, in no case shall control limits be greater than (closer to 100%) between 90 percent lagging and 95 percent leading.

Power factor control is typically required for distribution level generator interconnections where the generator is put on a power factor schedule, rather than a voltage schedule. Power Factor Control shall not be used for units connected to the transmission system.

**G2.9.6 Event Recorder**

All unattended generation facilities with capacity greater than 400 kW and with automatic or remotely initiated paralleling capability must have an event recorder that will enable PG&E to make an after-the-fact determination of the status of the Generation Facility at the time of the system disturbance, should such a determination be required. The events should be recorded to a one (1) milli-second resolution. In addition, the event recorder of generation facilities with a nameplate rating equal to or greater than 1,000 kW must also provide a record of deliveries to PG&E of real power in kW, reactive power in kVar and output voltage in kV.

**G2.10 SPECIAL PROTECTION SYSTEMS**

As stated in the NERC/WSCC Planning Standards, the function of a Special Protection System (SPS) is to “detect abnormal system conditions and take pre-planned, corrective action (other than the isolation of faulted elements) to provide acceptable system performance.” In the context of new generation projects, the primary action of a SPS would be to detect a transmission outage or an overloaded transmission facility and then trip or run back (reduce) generation output to avoid potential overloaded facilities or other criteria violations.

Any SPS proposal must be approved by both PG&E and CAISO and must comply with “ISO Grid Planning Guides for New Generator Special Protection systems” section of the California ISO Planning Standards.

**G2.11 REMEDIAL ACTION SCHEME (RAS) PARTICIPATION REQUIREMENT FOR GENERATION FACILITIES**

A RAS is a special protection system that automatically initiates one or more pre-planned corrective measures to restore acceptable power system performance following a disturbance. Application of RAS mitigates the impact of system disturbances and improves system reliability.

The output of electric generators may flow over the entire interconnected transmission system. A generation facility is therefore required to participate in remedial action schemes to protect local transmission lines and the entire system as PG&E determines necessary.
A typical disturbance, as it is considered in the planning and design of the electric transmission system, is the sudden loss of one or more critical transmission lines or transformers. A widely applied corrective measure is to instantaneously drop a sufficient amount of generation on the sending end of the lost transmission facility. This is known as generation dropping, and a participating generation facility may be disconnected from the transmission by the automatic RAS controller, in much the same way as by a transfer-trip scheme. A generation facility should therefore have full load-rejection capability as needed both for local line protection and RAS. The RAS design must be such that any single-point failure will not prevent the effective operation of the scheme.5

Whether RAS shall be required will depend on the overall location and size of the generator and load on the transmission system, the nature, consequences and expected frequency of disturbances and the nature of potential alternative transmission reinforcements.

G2.12 INDUCTION GENERATORS

Induction generators and other generators with no inherent Var (reactive power) control capability shall be required to provide an amount of reactive power equivalent to that required for a synchronous generator. They may also be required to follow a PG&E-specified voltage or Var schedule on an hourly, daily or seasonal basis, depending on the location of the installation. Specific instructions shall be provided by the Designated PG&E Electric Control Center (see Section G3).

Induction machines can be self-excited with the nearby distribution capacitors, or as the result of the capacitive voltage on the distribution network. Interconnecting facility should provide for a reclose block mechanism to avoid unintended operation of the unit following an outage on the distribution feeder to which it is interconnected.

G2.13 DC GENERATORS

G2.13.1 Inverters Capable of Stand-Alone Operation

Inverters capable of stand-alone operation are capable of islanding operation and shall have similar functional requirements as synchronous generators. For units less than 100 kW, usually it is acceptable to have the frequency and voltage functions built into the electronics of the inverter if the set points of these built-in protective functions are tamper-proof and can be easily and reliably tested. These relay functions must receive PG&E approval before they can be used to interconnect with the PG&E Power System. The total harmonic distortion in the output current of the inverters must meet ANSI/IEEE 519 requirements.

Inverter-type generators connected to the PG&E Power System must be pre-approved by PG&E. For units over 10 kW, a dedicated transformer will be required to minimize the harmonics entering into the PG&E Power System.

G2.13.2 Inverters Incapable of Stand-Alone Operation

Non-islanding inverters, rated 10 kW or less, that have met all the type tests and requirements for a utility interactive inverter found in UL 1741, have passed the additional tests outlined in the inverter certification section of Rule 21 and meet IEEE 519 harmonic requirements, are considered approved equipment for connection to PG&E. Inverters that do not meet the above requirements must meet the functional requirements of synchronous generators as outlined in this section.

5 System studies will determine the nature and intent of the RAS. Any RAS proposals to mitigate possible cascading outages outside the PG&E interconnection points or system requires review and approval by the appropriate WECC study groups and technical committees charged with detailed review.
G2.14 EMERGENCY GENERATOR REQUIREMENTS

There are two methods of transferring electric power supply between the PG&E source and the emergency generator system: open transition (break before make) and closed transition (make before break).

G2.14.1 “Break Before Make”:
This method can be accomplished via a double throw transfer switch or an interlock scheme that prevents the two systems from operating in parallel. The Generation Entity's main breaker shall not be allowed to close until the generator breaker opens. This open transition method does not require any additional protection equipment; however, it does cause the Generation Entity’s load to experience an outage while transferring back to PG&E. The length of this transfer depends on the transfer equipment.

G2.14.2 “Make Before Break”:
This method is used when the customer wants to minimize any loss of power or disturbance to the electric load. With this scheme, the customer's generator and the PG&E Power System are in parallel for a very short time interval during which the customer's load is being transferred between the PG&E source and the emergency generator. Both the transfer from PG&E to the emergency source and the transfer back can be accomplished without an outage.

G2.14.3 Interconnection Requirements:
Listed below are the requirements for the interconnection of emergency generators using the transfer schemes. First the general requirements for all transfer schemes are presented. Then the specific requirements for the two methods are listed.

G.2.14.3.1 Interconnection Protection Study
In general, a protection study is not required for these types of generation arrangements if the applicant meets the requirements outlined in this section and submits the required reports and drawings for review and approval.

G.2.14.3.2 Transfer Switch
The transfer switch must be rated for the maximum possible load current.

G.2.14.3.3 Notification and Documentation

1. The customer must notify PG&E in writing regarding all emergency generator installations, regardless of method of interconnection or transfer.

2. Complete documentation is required. Information should include but not limited to: a description of generator and control system operation, single line diagrams, identification of all interlocks, sequence of events description for transfer operation and specifications for any PG&E required protective devices.

3. All documentation must be approved by PG&E prior to installation.

4. Relay test reports must be reviewed and approved by PG&E 15 days prior to scheduling pre-parallel inspections.

G2.14.3.4 Operation/Clearance

1. For all line work and clearances, the emergency generator should be treated as a power source.

Note: This is a different study, not to be confused with a System Impact Study, see glossary for definitions
2. Customers utilizing “make before break” transfer schemes are required to notify the responsible Operation Center of their intent to transfer to their emergency generator and then again back to PG&E source, before any transfers are attempted. This notification is not required for break before make operation.

G2.14.3.5 “Break Before Make” Specific Requirements:

G2.14.3.5.1 Transfer Switch

The transfer switch must be of a design, or have an interlock, that prevents the transfer switch from closing and connecting the customer’s system with PG&E unless the emergency generator is already removed from the system.

G2.14.3.6 “Make Before Break” Requirements:

G2.14.3.6.1 Transfer Switch

1. The transfer switch must be rated for the maximum available fault duty in the event that the transfer switch closes into a fault condition.

2. There must be an interlock that will trip the main beaker or generator in the event of a failure of the transfer switch so that the unit will not remain paralleled to the PG&E Power System. This can be accomplished via a failure to open timer (see Table G2-5).

3. The controls for the transfer switch must prevent a parallel condition of the customer generator and the PG&E Power System from existing for an extended time period. Any system that allows a parallel to exist for greater than 0.5 seconds (30 cycles) on the transmission system and 1 second (60 cycles) on the distribution system should be subjected to an additional requirements outlined in other section of this document.

G2.14.3.6.2 Manual Disconnect:

1. The customer must provide a manual disconnect, located at the point of interconnection, which is used to establish a visually open safety clearance for the PG&E personnel working on the PG&E Power System.

2. The disconnect must be lockable in either the open or closed transition and operated only by PG&E.

3. The disconnect must be easily accessible, preferably located adjacent to the electric meter.

4. The disconnect must have full load break capability.

G2.14.3.6.3 Synchronizing Function:

The transfer scheme must have adequate control and protection to ensure the PG&E and customer electric systems are in synchronism prior to making the parallel. This is essential to ensure a safe and smooth transition. Synchronization is accomplished through the use of an auto-synchronizer or a synchronizing relay. The major requirements that these devices should possess are briefly listed below:

1. Slip frequency matching of 0.1 Hz or less.

2. Voltage matching of ± 10 percent or less.
3. Phase angle acceptance of ± 10 degrees or less.
4. Breaker closure time compensation.

G2.14.3.6.4 Protection:

Because the emergency generators are paralleled with the PG&E Power System, protective devices must be installed which will prevent the customer’s generator from remaining connected in the event of a fault occurring on the PG&E Power System during the transition. It is necessary to prevent damage to the customer’s equipment, the PG&E Power System, and other PG&E customers.

1. In most installations, the protection requirement may be satisfied through the installation of the reverse power relay (see Table G2-5). This relay should be installed on the customer’s side of the service transformer that is connected to the PG&E Power System. The relay should trip the customer’s main breaker and must be able to detect transformer core magnetizing power. In this manner, reverse power flow is detected before it actually enters the PG&E Power System and other customers’ equipment. This can be accomplished by setting the current level pick up equivalent to 60 percent of the transformer bank magnetizing current. Because this current value will be small, the current transformers associated with the relay must be capable of providing these small currents.

2. When transferring the customer’s load back to the PG&E Power System. It is possible to have incidental power flow back to PG&E’s system. By properly setting the synchronizing and/or generator control, this reverse flow can be avoided. However, a short time delay may be required on the reverse power relay to prevent it from tripping the generator unnecessarily each time a transfer is attempted. At no time should this time delay exceed one second.

G2.14.3.6.5 Dedicated Transformer

Due to the fact that the emergency generator is connected in parallel with the PG&E Power System, all transfer schemes of this type must have a dedicated transformer. This will lessen the possibility that any transfer activities will affect other PG&E customers. In addition, a dedicated transformer is also necessary to allow the installation of the reverse power relay scheme.

G2.15 PARALLEL-ONLY (NO SALE) GENERATOR REQUIREMENT

Parallel-Only generators shall have similar requirements as that of any other standard synchronous generator interconnection except that PG&E may at its discretion allow the installation of three very sensitive, single-phase, reverse power relays (such as the Basler BE1-32R) along with the dedicated transformer as an alternative to the normally required ground relays. The reverse power relays shall be set to pick up on transformer magnetizing current with a time delay not to exceed 0.5 second. This option may not be feasible on generating systems with a slow load rejection response since they may be tripped off-line frequently for in-plant disturbances.

Owners of Parallel-Only generators, particularly Rule 21 customers must execute a parallel-only operating agreement with PG&E prior to operation by the generation owner.
G2.16 GENERATION ENTITY-OWNED PRIMARY OR TRANSMISSION VOLTAGE TAP LINES (60 KV AND ABOVE)

If the Generation Entity constructs, owns and maintains a transmission-level voltage tap line extension, the entity shall also install, own and maintain the following equipment at the point of interconnection with PG&E:

- The fault-interrupting protection device; i.e., breaker, recloser, as specified by PG&E.
- The manual isolating disconnects (gang-operated).
- High-side metering installation as outlined in Section G1.

G2.17 PG&E PROTECTION AND CONTROL SYSTEM CHANGES WHICH MAY BE REQUIRED TO ACCOMMODATE GENERATOR INTERCONNECTION

At the Generation Entity's expense, PG&E will perform a detailed interconnection study to identify the cost of any required modifications to PG&E's protection and control systems that are required to interconnect a new generation source. Retail generators will execute a Generation Special Facilities Agreement (Appendix L) as indicated in Electric Rule 21 to recover the costs to PG&E associated with any protection and control system modifications which are directly assigned to the Generation Entity. Wholesale generators will execute a FERC-jurisdictional Generator Interconnection Agreement.

These protection and control system modifications are in addition to any transmission system upgrades identified in the system impact or facilities studies for interconnection of the new generation facility.

Following is a partial list of protection system modifications that may be required:

- PG&E’s automatic restoration equipment shall be prevented from operating until the generator is below 25 percent of nominal voltage as measured at the restoration equipment (Figure G2-9). Generator damage and system disturbances may result from the restoration of power by automatically re-energizing PG&E's facilities. This modification shall be required when the generator(s) has the capability of energizing a line when the PG&E Power System is disconnected. PG&E will not allow the Generation Entity's generator(s) to automatically re-energize PG&E facilities.

- For generation facilities greater than 1,000 kW aggregate nameplate rating, all existing single phase fault interrupting devices (fuses) located in series between the generator and PG&E's substation, shall be replaced with three phase interrupting device to prevent possible single-phasing of other customers.

- The PG&E substation transformer high side fuses must be replaced with a three-phase interrupting device when the generator is on a distribution circuit fed from a fused PG&E substation transformer bank, and the bank's minimum load is equal to or less than 200 percent of the generator's nameplate rating.

- Installation of transfer trip from the high-side circuit breaker/circuit switcher, as well as the distribution breaker and any line reclosers, to the generator if found necessary by PG&E. An associated EMS/SCADA telemetering circuit is required between the Generation Entity’s site and the Designated PG&E Electric Control Center.

G2.18 DIRECT TELEPHONE SERVICE

The Generation Entity must obtain direct service from the local telephone company for a business telephone so that operating instructions from PG&E can be given to the designated operator of the Generation Entity's equipment. In addition, another telephone must be available near the protection equipment and telemetering equipment. This telephone would be used for maintenance.
of the various data a protection system that may be in service. Other types of leased circuits would include protection and EMS/SCADA data circuits.

Communications circuits for transfer trip and EMS/CADA must be in service at least three weeks prior to connection to the PG&E power grid. It is critical to the project schedule that the required leased circuits are ordered many months in advance of the operational date. In Appendix F, approximate timeframes are provided for different types of circuits and services. These are approximate lead times for planning purposes. The telephone company will need to determine whether adequate cable pair facilities are available at each facility for the required service. If cable plant is not available, the generator should plan on 6-12 months before having the service.

A Telephone line may also be required for remote metering at the Gas Valve location as appropriate. PG&E telecommunications personnel should evaluate this installation to make sure that the proper precautions are taken to ensure that the dielectric strength of the cable and protection equipment at the termination points of the cable are adequate to meet safety criteria.

G2.19 STANDBY STATION SERVICE
Contact PG&E’s local representative if the Generation Entity desires standby service for station use.

G2.20 STATION BATTERY
A stationary battery, either a flooded lead acid type or NiCd type, is required to power utility grade relays and for tripping the breaker. For detailed requirements about type, calculations and design, and test reports, etc., please refer to Appendix T: Battery Requirements for Interconnection to PG&E System
### Table G2-1

#### STANDARD DEVICE NUMBERS

<table>
<thead>
<tr>
<th>Device Number</th>
<th>Definition and Function</th>
<th>Device Number</th>
<th>Definition and Function</th>
</tr>
</thead>
<tbody>
<tr>
<td>15</td>
<td>Speed of frequency matching device is a device that functions to match and hold the speed or the frequency of a machine or of a system equal to, or approximately equal to, that of another machine, source or system.</td>
<td>46</td>
<td>Reverse-phase or phase-balance, current relay is a device which functions when the polyphase currents are of reverse-phase sequence, or when the polyphase currents are unbalanced or contain negative phase sequence components above a given amount.</td>
</tr>
<tr>
<td>21</td>
<td>Distance Relay is a device which functions when the circuit admittance, impedance, or reactance increases or decreases beyond predetermined limits.</td>
<td>47</td>
<td>Phase-sequence voltage relay is a device that functions upon a predetermined value of polyphase voltage in the desired phase sequence.</td>
</tr>
<tr>
<td>25</td>
<td>Synchronizing, and synchronism-check, device operates when two a-c circuits are within the desired limits of frequency, phase angle and voltage, to permit or to cause the paralleling of these two circuits.</td>
<td>50</td>
<td>Instantaneous overcurrent, or rate-of rise relay is a device which functions instantaneously on an excessive value of current, or on an excessive rate of current rise, thus indicating a fault in the apparatus or circuit being protected.</td>
</tr>
<tr>
<td>27</td>
<td>Undervoltage relay is a device that functions on a given value of undervoltage.</td>
<td>51</td>
<td>A-C time overcurrent relay is a device with either a definite or inverse time characteristic that functions when the current in an a-c circuit exceeds a pre-determined value.</td>
</tr>
<tr>
<td>32</td>
<td>Reverse power relay is one which functions upon a reverse power flow at a given set point.</td>
<td>52</td>
<td>A-C circuit breaker is a device that is used to close and interrupt and a-c power circuit under normal conditions or to interrupt this circuit under fault or emergency conditions.</td>
</tr>
</tbody>
</table>
### Table G2-1

**STANDARD DEVICE NUMBERS**

(Continued)

<table>
<thead>
<tr>
<th>Device Number</th>
<th>Definition and Function</th>
<th>Device Number</th>
<th>Definition and Function</th>
</tr>
</thead>
<tbody>
<tr>
<td>59</td>
<td>Overvoltage relay is a device that functions on a given value of overvoltage.</td>
<td>79</td>
<td>A-C reclosing relay is a device that controls the automatic reclosing and locking out of circuit interrupter.</td>
</tr>
<tr>
<td>60</td>
<td>Voltage balance relay is a device which operates on a given difference in voltage between two circuits.</td>
<td>81</td>
<td>Frequency relay is a device that functions on a predetermined value of frequency—either under or over the normal system frequency—or rate of change of frequency.</td>
</tr>
<tr>
<td>61</td>
<td>Current balance relay is a device that operates on a given difference in current input or output of two circuits.</td>
<td>87</td>
<td>Differential protective relay is a protective device which functions on a percentage or phase angle or other quantitative difference of two currents or of some other electrical quantities.</td>
</tr>
<tr>
<td>62</td>
<td>Time-delay stopping, or opening, relay is a time-delay device which serves in conjunction with the device which initiates the shutdown, stopping, or opening operation in an automatic sequence.</td>
<td>90</td>
<td>Regulating device functions to regulate a quantity, or quantities, such as voltage, current, power, speed, temperature, frequency, and load, at a certain value or between certain limits for machines, tie lines, or other apparatus.</td>
</tr>
<tr>
<td>67</td>
<td>A-C directional overcurrent relay is a device that functions on a desired value of a-c overcurrent flowing in a predetermined direction.</td>
<td>94</td>
<td>Tripping or trip-free relay is a relay that functions to trip a circuit breaker, contactor, or equipment, or to permit immediate tripping by other devices; or to prevent immediate reclosure of a circuit interrupter if it should open automatically even though its closing circuit is maintained closed.</td>
</tr>
</tbody>
</table>
## RELAY TEST REPORT

<table>
<thead>
<tr>
<th>FACILITY NAME</th>
<th>TESTING BY</th>
<th>DATE INSTALLED</th>
<th>LOCATION</th>
<th>DATE LAST TESTED</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>FIRM</td>
<td></td>
<td>ADDRESS</td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>FACILITY ACCOUNT NUMBER</th>
<th>TESTED FOR INSTALLATION</th>
<th>ROUTINE</th>
<th>OTHER</th>
</tr>
</thead>
</table>

### RELAY INFORMATION

<table>
<thead>
<tr>
<th>DEVICE NO</th>
<th>FUNCTION</th>
<th>MFR.</th>
<th>TYPE</th>
<th>STYLE</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>TIME RANGE</th>
<th>INST. RANGE</th>
<th>CT RATIO</th>
<th>PRI. MIN.</th>
<th>PRI. INST.</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>OHMIC RANGE @ ANGLE</th>
<th>OFFSET</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>DEVICE NO</th>
<th>FUNCTION</th>
<th>MFR.</th>
<th>TYPE</th>
<th>STYLE</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>TIME RANGE</th>
<th>INST. RANGE</th>
<th>CT RATIO</th>
<th>PRI. MIN.</th>
<th>PRI. INST.</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>CT RATIO</th>
<th>PRI. MIN.</th>
<th>PRI. INST.</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### DIRECTIONAL ELEMENTS:

<table>
<thead>
<tr>
<th>DEVICE NO</th>
<th>DEVICE NO</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### CONTACTS:

- CLOSED TO OPEN AT: (Deg. I Lag E)
- OPEN TO CLOSED AT: (Deg. I Lag E)
- MAXIMUM TORQUE AT: (Deg. I Lag E)
- MIN. P.U.: EXI:

### MIN. P.U.: EXI:

<table>
<thead>
<tr>
<th>INDEX</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
</tr>
</tbody>
</table>

### TIME ELEMENTS:

<table>
<thead>
<tr>
<th>TIMES TAP</th>
<th>CURVE</th>
<th>TEST</th>
</tr>
</thead>
<tbody>
<tr>
<td>A PHASE</td>
<td>B PHASE</td>
<td>C PHASE</td>
</tr>
</tbody>
</table>

### TIMES TAP CURVE TEST TIMES TAP CURVE TEST

<table>
<thead>
<tr>
<th>TIMES TAP</th>
<th>CURVE</th>
<th>TEST</th>
</tr>
</thead>
<tbody>
<tr>
<td>A PHASE</td>
<td>B PHASE</td>
<td>C PHASE</td>
</tr>
</tbody>
</table>

### INST. P.U. CURRENT INST. P.U. CURRENT

| PRIMARY "ONE-SECOND" GROUND CURRENT (JOINT POLE) |
| TIME ELEMENTS: |
| TIMES TAP | CURVE | TEST |
| A PHASE   | B PHASE | C PHASE |

### PRIMARY "ONE-SECOND" GROUND CURRENT (JOINT POLE)

<table>
<thead>
<tr>
<th>INST. P.U. CURRENT</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
</tr>
</tbody>
</table>
Form G2-2

(Continued)

<table>
<thead>
<tr>
<th>STATION</th>
<th>SW. NO.</th>
<th>DATE INSTALLED</th>
<th>DATE LAST TESTED</th>
<th>MFR.</th>
<th>TYPE</th>
<th>RATING</th>
<th>AMPS</th>
<th>KV</th>
</tr>
</thead>
<tbody>
<tr>
<td>OPERATOR: TYPE</td>
<td>MODEL</td>
<td>INTERRUPTING RATING</td>
<td>SW. COUNTS ON</td>
<td>N.P. VOLTS TO CLOSE</td>
<td>TRIP</td>
<td>WIND/PUMP</td>
<td>C VOLTS AT SW.</td>
<td>MIN. VOLTS TO CLOSE</td>
</tr>
<tr>
<td>AMMETER</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>WATTMETER</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>VARMETER</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>RECLOSEING RELAY: DEVICE NO.</td>
<td>RESTORE POWER</td>
<td>PARALLEL</td>
<td>MFR.</td>
<td>STYLE</td>
<td>TEST LINE</td>
<td>LOCKOUT</td>
<td>MODIFIED PER DWG. NO.</td>
<td>BANK/BUS TEST</td>
</tr>
<tr>
<td>ADDITIONAL RELAY DATA</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>DEVICE NO.</td>
<td>MFR.</td>
<td>TYPE/STYLE</td>
<td>RATING</td>
<td>USED FOR</td>
<td>VOLTS, AMPS OR TIME</td>
<td>OPERATE</td>
<td>RESET</td>
<td></td>
</tr>
<tr>
<td>REMARKS:</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Pacific Gas and Electric © 2004
Table G2-4  
RELAYS FOR GENERATION APPLICATION\textsuperscript{2,4}  
(For Directional Overcurrent and Distance Relays, refer to Table G2-5)  
(See notes on following page)

<table>
<thead>
<tr>
<th>DEVICE</th>
<th>Synch Check Relay</th>
<th>Synchronizing Relay\textsuperscript{17}</th>
<th>Automatic Synchronizer\textsuperscript{7}</th>
<th>Undervoltage Relay\textsuperscript{15}</th>
<th>Non-directional Overcurrent Relay</th>
<th>Non-directional Overcurrent Relay Ground</th>
<th>Overcurrent with Voltage Restraint or Voltage Control</th>
<th>Overvoltage Relay \textsuperscript{15}</th>
<th>Overvoltage\textsuperscript{5} Ground Fault Detection (Neutral)</th>
<th>Frequency Relay (Under/Over)</th>
<th>Under, Over, &amp; Reverse Power\textsuperscript{13}</th>
<th>Time Delay</th>
</tr>
</thead>
<tbody>
<tr>
<td>Device Number</td>
<td>25 25 15/25 27 50/51 5N 51V\textsuperscript{5,6,8} 59 59N 81U/O 32 62</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>MANUFACTURER</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>ABB (ASEA) (Westinghouse)</td>
<td>RXEG CV RXIDF CO DPU-2000R Microshield (MSOC) RXIDF CO DPU-2000R COV RXEG SV COV8 RXFE RXKE RXKD TD</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>AREVA MAVS</td>
<td>MCGG MCGG MiCOM P921, P923 MiCOM P921, P923 MVTT</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Basler Electric BE1-25 BE1-GPS\textsuperscript{13} BE1-IPS</td>
<td>BE1-25A BE1-27 BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS} BE1-GPS \textsuperscript{BE1-IPS}</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Cooper</td>
<td>IDP-210 iDP-210 iDP-210 iDP-210 iDP-210 iDP-210 iDP-210</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Cutler Hammer</td>
<td>IQ Transfer</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

\textsuperscript{2} For Directional Overcurrent and Distance Relays, refer to Table G2-5.  
\textsuperscript{4} See notes on following page.

Pacific Gas and Electric © 2006
<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>General Electric (Multilin)</td>
<td>D-60</td>
<td>SASB</td>
<td>1AV</td>
<td>IAV</td>
<td>IFC</td>
<td>IFC</td>
<td>IFCV</td>
<td>IFV</td>
<td>IAV</td>
<td>SFF</td>
<td>SR-489</td>
<td>SAM</td>
</tr>
<tr>
<td>Schweitzer</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td>SEL-300G, SEL-311C, SEL-311L</td>
<td>SEL-300G</td>
<td>SEL-300G</td>
<td></td>
</tr>
<tr>
<td>SEL-311C</td>
<td></td>
<td></td>
<td>SEL-311C</td>
<td>SEL-311C</td>
<td>SEL-311C</td>
<td>SEL-311C</td>
<td>SEL-311L</td>
<td>SEL-311L</td>
<td>SEL-311C, SEL-311L</td>
<td>SEL-311L</td>
<td>SEL-311L</td>
<td></td>
</tr>
<tr>
<td>SEL-321</td>
<td>SEL-351</td>
<td></td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td>SEL-351</td>
<td></td>
</tr>
<tr>
<td>Woodward</td>
<td>SPM 9905-005</td>
<td>DSLC, MSLC, DSM 9905-204</td>
<td>1AV</td>
<td>IAV</td>
<td>IFC</td>
<td>IFC</td>
<td>IFCV</td>
<td>IFV</td>
<td>IAV</td>
<td>SFF</td>
<td>SR-489</td>
<td></td>
</tr>
</tbody>
</table>
Notes for Table G2-4:

1. Generation requiring three underfrequency set points may necessitate an additional underfrequency device.

2. All microprocessor-based relays that are applied as a multifunctional protection device will require backup relays. (Alternate or backup protective relays can be electromechanical, solid state, or microprocessor based relays.) Most microprocessor relays include event reporting and fault locating functions. Relay settings, sequences of events listing, and fault records should not be lost or revert to default values when DC source is momentarily lost. Event and Oscillography should not be erased from the relay records when the front panel reset button is exercised to reset the Target LCD display.

3. Voltage restrained overcurrent relays are preferred; however, if no problems with protective coordination occur, voltage controlled relays may be used. An auxiliary potential transformer is required for the 51V if the main interconnecting transformer is a wye-delta bank and the relay does not automatically adjust for appropriate phase shift.

4. The above table contains information regarding specific products, manufacturers and representatives. These tables are not all inclusive. The inclusion or omission of products, a manufacturer or representative is not meant to be an indication of the quality or reliability of a product or service. No endorsements or warranties are implied. Other types of relays may be acceptable but certified test results performed by an independent party must be reviewed and approved by PG&E prior to installation and commercial operation.

5. Refer to the notes on Table G2-5 for a list of approved relays used in open delta ground sensing schemes. Relay should have the magnetic measurement inputs specifically designed to support multiple required tasks. For example, multiple independent relays are required to meet the complements of reverse power, synchronizing check, and ground fault detection overvoltage functions.

6. Distance characteristic relays can be used as an alternate to using voltage restraint relays when system conditions coupled by unit characteristics permit.

7. Synchronizing devices must be ordered with the following option: a) voltage matching, b) phase angle acceptance, c) slip frequency acceptance, and d) breaker time compensation.

8. Three single phase units are implied, a single three-phase overcurrent relay is acceptable if a redundant system is provided. There may be occasions when a three-phase 51V/27R relay may not be applicable.

9. Manual synchronization with synch-check relay and synchroscope only allowed for generators with less than 1000kW aggregate nameplate rating.

10. The Beckwith M-0193 and M-0194 work in conjunction to provide the Automatic Synchronizer function.

11. The Basler BE1-32R has been superceded by the reverse power feature on the devices in this column. For reverse power applications, the relay sensitivity should be evaluated to meet the transformer magnetizing current requirements for reverse power, see Appendix R.

12. Basler BE1-GPS and Beckwith M3410 have 3 phase measuring power elements. Basler BE1-IPS and Beckwith M3410A and M3520 have three single-phase measuring elements for power measurements and protection computations. Refer to note 11 prior to selection of the devices as different relays have different measuring sensitivity elements. For example, Beckwith M3410A sensitivity is approximately 0.75 mA of real power component, where as Beckwith M-3520 has a sensitivity of 10mA of real component current. The IPS 32 function is suitable for low forward type detection and is suitable for conditions where the power factor is greater than 0.1.

13. The over / under power function of the Basler IPS has user settable 32 setting element that can utilize combination of 1 of 3, 2 of 3, 3 of 3, or total 3-phase power. Verify the user has three phase-to-neutral voltage sources and the relay is set to the 1 of 3 phase power option to meet PG&E’s single phase over / under power requirements.

14. Auxiliary voltage measuring element is required to make use of the Basler BE1-GPS synchronizing check setting option.

15. Multi-function devices in this column have the features that may be utilized provided that the voltage source is utilized. The voltage sensing logic in different styles from the same manufacturer or between different manufacturers may not have capability for loss of voltage detection to alarm, when single phase voltage is used.

16. All relays must have 5A nominal AC input current.

17. For SEL-351-7 verify that the application meets the minimum sensitivity of the relay before selection. The minimum sensitivity of the relay is 3.5 watts secondary (0.05 amps @70v single phase). This relay is approved for Rule 21 "Minimum Import" applications for settings no less than 4 watts secondary. In general, the relay is not approved for reverse power applications (0.1% of bank rating) unless calculations demonstrate that it can be set above the minimum sensitivity.
### Table G2-5

**Relays for Generation Interconnection Application**

(For Voltage, Overcurrent, and Frequency Relays, See Table G2-4)

(See notes on following page)

<table>
<thead>
<tr>
<th>DEVICE</th>
<th>Distance Relay Zone 1</th>
<th>Distance Relay Zone 2 Pilot Protection</th>
<th>Distance Relay Zone 3 Blocking Pilot</th>
<th>Distance Relay Gnd Distance</th>
<th>Directional Time Overcurrent Phase</th>
<th>Directional Time Overcurrent Ground</th>
<th>Directional Overcurrent Pilot (Phase and Ground)</th>
<th>Current Differential or Phase Comparison</th>
<th>Auxiliary</th>
</tr>
</thead>
<tbody>
<tr>
<td>DEVICE NUMBER</td>
<td>21</td>
<td>21Z2</td>
<td>21Z2C</td>
<td>21Z3C</td>
<td>21Z2G</td>
<td>67</td>
<td>67N</td>
<td>67NC</td>
<td>87L / 78</td>
</tr>
<tr>
<td>MANUFACTURER</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>AREVA</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
<td>OPTIMHO QUADRAMHO</td>
</tr>
<tr>
<td>Basler Electric</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Beckwith</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
<td>M3425</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Schweitzer</td>
<td>SEL 221F</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
<td>SEL 221G</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Pacific Gas and Electric © 2004

G2-30

8/6/07
Notes for Table G2-5

- The above table contains information regarding specific products, manufacturers and representatives. This table is not all-inclusive. The inclusion or omission of a product, manufacturer or representative is not meant to be an indication of the quality or reliability of a product or service. No endorsements or warranties are implied. Only PG&E approved relays may be installed for protection of interconnecting distribution or transmission lines. Refer to Appendix F for direct transfer trip (DTT) and pilot protection requirements when applicable.

- Most microprocessor relays include event reporting and fault locating functions. Relay settings, event, and fault records should not be lost or revert to default values when DC source is momentarily lost. Event and Oscillography should not be erased from the relay records when the front panel reset button is exercised to reset the Target LCD display.

- All microprocessor based relays being used as a multifunctional protection device will require backup relays, except for generation less than 400 kW aggregate nameplate with relay failure output contract connected to trip the generation breaker. (Alternate or backup protective relays can be electromechanical, solid state, or microprocessor based relays.)

- Primary and alternate protective devices must utilize different operating principals and not be subject to possible common mode failures in order to minimize the potential for insufficient interconnection protection, where applicable, or unnecessary plant shut down; for example, due to possible product advisory letters issued by the manufacturers.

- Neutral or broken delta ground detection relays approved for interconnection are ABB CV-8 and GE IAV and I

- All relays must have 5A nominal AC input current.
### Table G2-6

**OVERFREQUENCY AND UNDERFREQUENCY RELAYS**

**OVERVOLTAGE AND UNDERVOLTAGE RELAYS**

**Transmission System Interconnection**

<table>
<thead>
<tr>
<th>Description of Facility</th>
<th>Over Frequency</th>
<th>Under Frequency</th>
<th>Over(^3) Voltage (% of Nominal)</th>
<th>Under(^4) Voltage (% of Nominal)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Generation of 100 kW or Less</td>
<td>62.0 Hz @ 1 sec</td>
<td>58.0 Hz @ 30 sec</td>
<td>120</td>
<td>80</td>
</tr>
<tr>
<td>Generation &gt; 100 kW (except hydro generators using three set point relay)</td>
<td>63.0 Hz @ 30 cycles</td>
<td>58.4 Hz @ 1.5 min 58.0 Hz @ 30 sec 57.6 Hz @ 7.5 sec</td>
<td>120</td>
<td>80</td>
</tr>
<tr>
<td>Generation &gt; 100 kW (hydro generators only using single set point relay)</td>
<td>63.0 Hz @ 30 cycles</td>
<td>54.0 Hz @ 6 cycles</td>
<td>120</td>
<td>80</td>
</tr>
<tr>
<td>Generation &gt; 100 kW (non-hydro induction generators using single set point relays)</td>
<td>63.0 Hz @ 30 cycles</td>
<td>55.0 Hz @ 6 cycles</td>
<td>120</td>
<td>80</td>
</tr>
<tr>
<td>Generation &gt; 100 kW (using single set point relay except hydro and induction generators)</td>
<td>63.0 Hz @ 30 cycles</td>
<td>57.0 Hz @ 0 cycles</td>
<td>120</td>
<td>80</td>
</tr>
</tbody>
</table>

**Notes:**

1. Underfrequency relays shall be set no higher than the recommended settings above.
2. Generators 75 MW and larger must use underfrequency relay with three set points. For generators greater than 100 kW and less than 75 MW, except hydro generators, an underfrequency relay with three set points is recommended.
3. The overvoltage relay is set to initiate a trip of the circuit breaker without an intentional time delay when the voltage is equal or above the stated percent of normal.
4. For undervoltage relays, set time delay typically at 3 to 5 seconds at zero voltage to allow for motor starting and for coordination of line protection devices.
5. All settings meet the WECC underfrequency requirement.